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APPLICATION FOR LETTERS PATENT

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SEMICONDUCTOR PROCESSING SPRAY  
COATING APPARATUS

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## CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation-in-part of copending U.S. Patent Application Serial No. 07/855,767 filed March 18, 1992; which is a continuation-in-part of U.S. Patent Application Serial No. 07/665,942 filed March 6, 1991 (now U.S. Patent No. 5,235,995).

Priority under 35 U.S.C. §120 is claimed based upon the above applications which are also hereby incorporated by reference.

## TECHNICAL FIELD

This invention relates to apparatus and methods for coating semiconductor wafers, flat panel displays, data disks, microelectronic components, thin film heads for hard disk drives, and other microelectronic or semiconductor articles that must be coated with a relatively uniform confirmation coating layer over irregular surfaces.

## BACKGROUND OF THE INVENTION

The production of semiconductor devices, such as semiconductor wafers, semiconductor substrates, flat panel displays, data discs and other similar articles, generally requires at least one step in which a coating must be applied in a uniform layer across a surface of the device. For instance, the production of integrated circuits frequently involves the application of a uniform coating of photoresist on a silicon wafer or substrate.

1 The small feature size and variety of micro-devices being produced  
2 need highly uniform coating layers to be produced. The production of  
3 micro-devices is significantly affected by current limitations associated  
4 with non-uniformity in coating layers, particularly when coating over  
5 irregular surfaces. Such irregular surfaces occur due to the micro-  
6 devices having one or more features such as vias, channels, and peaks.  
7 These features produce irregularities in the height of the surface over  
8 which the coating is being applied. These surface irregularities cause  
9 problems and limit the overall production performance and effectiveness  
10 of conventional coating apparatus and methods because the coatings  
11 cannot be applied in a sufficiently uniform manner. The coatings often  
12 fill channels, run off the peaks, and in some instances are unable to  
13 adequately fill vias. As a result, the coating layer is thickened in the  
14 channels, and thinned on the peaks. Vias can either be underfilled or  
15 overfilled depending upon viscosity and feature geometry.

16 A common prior art technique for applying photoresist coatings  
17 involves spraying the wafer with a photoresist and then spinning the  
18 wafer. The spinning action of the wafer produces centrifugal forces  
19 which spread the liquid photoresist. However, these spin application  
20 techniques have difficulties in providing layers having good uniformity.  
21 Striations are a common problem. These striations can be initiated by  
22 surface features, contaminants, or fluid properties of the coating being  
23 applied. These and other irregularities have derogatory effects on the  
24 production of micro-circuits and other micro-devices.

1 Prior art semiconductor coating techniques have not been able to  
2 provide thin, uniform coating layers which conform to irregularities  
3 present on the wafer or other semiconductor surface being coated. Spin  
4 coating techniques produce coating layers which tend to have an  
5 approximately level or planar surface even though surface features of  
6 varying heights are contained beneath the coating. The surfaces of  
7 wafers can contain topographical height variations of 10-40 microns with  
8 associated horizontal increments of 100-500 microns. Coatings  
9 thicknesses can thus vary in the range of 5-30 microns. This creates  
10 variations in the width of lines or other critical dimensions. These  
11 variations can in turn cause significant process yield losses. Thus, there  
12 is a need for improved coating apparatus and methods which can  
13 produce a coating layer onto semiconductor surfaces which is  
14 conformational to provide more uniform coating thickness, even when  
15 applied over surfaces having features of varying heights and shapes.

16 Prior art coating techniques have also been troubled by difficulties  
17 which arise during lithographic processes performed upon coating layers.  
18 These difficulties arise when coating thicknesses vary to a degree  
19 sufficient to cause focusing variations in the lithographic beams used to  
20 define features of a device. These problems are in particular significant  
21 when complex topographical configurations are used. This increased  
22 difficulty occurs due to the greater difficulty in producing uniform  
23 coating thicknesses on complex topographical configurations.  
24

1 Prior art semiconductor coating equipment and techniques have  
2 also been deficient in not providing uniform application of relatively  
3 viscous coating materials. The exact mechanism causing the difficulties  
4 are not fully understood. This problem of coating with viscous coatings  
5 is further exacerbated when the surface being coated is irregular, such  
6 as discussed above.

7 The application of coatings to semiconductor article surfaces is  
8 further complicated by the extraordinarily low levels of contamination  
9 which must be maintained when processing semiconductor materials.  
10 Contaminating particles will cause defects to exist in the resulting  
11 products and will typically decrease device yields and profitability. Thus  
12 there is a strong need to produce uniform coating layers free from  
13 contaminants or congealed particulate accumulations which may form  
14 from the coating materials themselves.

15 Another problem associated with present equipment and methods  
16 for coating semiconductor wafers and similar devices is that a relatively  
17 large volume of coating material is used. This occurs in some instances  
18 because the coating is applied and the wafer is spun to provide  
19 centrifugal dispersion of the coating across the wafer surface. This  
20 leads to coating material being spun off and wasted. In other  
21 equipment the coating spray is not efficiently applied and is wasted in  
22 part as an aerosol of coating particles which do not adhere to the  
23 surface being coated.  
24

1 A further problem associated with current techniques is inefficient  
2 coating application equipment and techniques. The excess coating  
3 material is either wasted, or else time and money are expended to  
4 dispose of, reformulate, or recycle the spent coating material. Thus  
5 there is a continuing need for methods and apparatus which can more  
6 precisely coat such articles using a relatively smaller amount of coating  
7 material and with reduced waste.

8 For these and other reasons, there is a strong need for improved  
9 methods and apparatus which can provide a uniform coating layer on  
10 irregular semiconductor article surfaces using reduced amounts of the  
11 coating materials.

#### 12 13 BRIEF DESCRIPTION OF THE DRAWINGS

14 Preferred embodiments of the invention are described below with  
15 reference to the accompanying drawings, which are briefly described  
16 below.

17 Fig. 1 is a front elevational view showing a preferred wafer spray  
18 coating and processing system made in accordance with the concepts of  
19 this invention.

20 Fig. 2 is a top view showing the system of Fig. 1. Portions have  
21 been removed to better show features of the invention.

22 Fig. 3 is a side sectional view showing portions of a spray  
23 processing vessel bowl used in the system of Fig. 1. A spray  
24 processing vessel head is shown in phantom lines.

1 Fig. 4 is a side sectional view of the spray processing vessel head  
2 shown in phantom in Fig. 3. The section line is taken along a cutting  
3 plane which changes at the centerline of the rotating assembly to better  
4 show internal components.

5 Fig. 5 is a top view of the spray processing vessel bowl shown  
6 in Fig. 3.

7 Fig. 6 is a front elevational view of a thermal treatment station  
8 used in the system of Fig. 1.

9 Fig. 7 is a top view of a one thermal treatment unit used in the  
10 thermal treatment station shown in Fig. 6.

11 Fig. 8 is a sectional view along section line 8-8 of Fig. 7.

12 Fig. 9 is a top view of an alternative spray-head having multiple  
13 nozzles.

14 Fig. 10 is a schematic diagram showing fluid components  
15 associated with the spray coating station.

16 Fig. 11 is a schematic block diagram showing control system  
17 components.

## 18 19 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

20 This disclosure of the invention is submitted in furtherance of the  
21 constitutional purposes of the U.S. Patent Laws "to promote the  
22 progress of science and useful arts" (Article 1, Section 8).  
23  
24

## System Generally

Fig. 1 shows a preferred semiconductor spray coating processing system 10 built in accordance with the novel concepts of this invention. Processing system 10 includes a frame or framework 11 upon which other components are mounted. Framework 11 and remaining portions of the processor are advantageously supported on rollable casters 14.

Framework 11 is advantageously constructed so as to provide a control side or section 12 and a wafer processing side or section 13. The processing side has a processing compartment 15 which encloses a work space. Processing compartment 15 includes several system stations which receive and process semiconductor substrates, semiconductor wafers, flat panel displays, data disks, and other semiconductor products or articles requiring ultra-low contamination processing. The processing accomplished by processing system 10 includes spraying a desired coating upon the articles. Below the processing compartment 15 is an equipment storage compartment 16 wherein various components of the system and consumable supplies, such as liquid coating materials are stored.

Processor 10 includes a front 18 which has several removable access panels 28 which are detachable from frame 11 by opening catches 29. Similar panels are used on the sides 20 and 22, and back 21 of the processor. Processor 10 also includes a top 19. The top processing side has been removed in the view shown in Fig. 2. This



top panel preferably has a window (not shown) for viewing into the processing compartment.

Fig. 1 shows that the processing side 13 further has an access door 24 which is pivotally connected to a front panel of the processing compartment using hinges 26. Door 24 preferably has a view window 25 for operator observation of the processes being performed within processing compartment 15 during operation.

Fig. 1 also shows frontal portions of the control side 12 of processor 10. Primary portions of a control subsystem 30 is mounted within control side 12. Illustrated components include a display 31 which is a touch screen cathode ray tube, known in the art. A data disk drive 32 is mounted below the display. A keyboard connection port 34 allows a keyboard to be connected for purposes of programming the controller. An emergency stop button 33 is mounted for easy access to allow the operator to stop operation of the machine for any reason. The control subsystem 30 includes a computer or other central controller 300 such as typically used in a variety of offices and industrial control situations. The control system computer 300 interfaces through connection wiring and in some cases related electronic subcircuits to both monitor system operation and provide operational control signals. Fig. 11 shows the relationships in a schematic diagram. The specific control scheme used can vary significantly according to well-known digital control options available to provide the operational capabilities described below in greater detail.

Fig. 2 shows the top of processor 10. The processing compartment 15 is shown with the top cover 27 removed for purposes of illustration. The processing compartment top cover 27 also includes an exhaust port 48 (Fig. 1) through which gases emanating from the processing compartment can be withdrawn, such as to a facilities exhaust line (not shown).

### Wafer Transfer

Fig. 2 includes a processing compartment deck 23. Deck 23 is supported by the framework and in part supports various components which are mounted in or adjacent to the processing compartment. As shown, deck 23 mounts a robotic wafer transfer station 41. Wafer transfer station 41 has a base 64 which is mounted upon deck 23. The wafer transfer mechanism also includes a first arm 65 which is pivotally connected to base 64 at a proximate end of the first arm. Arm 65 is vertically adjustable relative to the base using an extension cylinder 42. A second arm 66 has a proximate end which is pivotally connected to the distal end of first arm 65. The distal end of second arm 66 carries a wafer engagement tool 67. The wafer engagement tool is preferably mounted to allow pivotal action of the engagement tool relative to the distal end of second arm 66. The wafer engagement tool is advantageously a vacuum assisted end effector which is inserted beneath a wafer and applies a vacuum to the wafer backside to hold the wafer in position upon the palm or upper face of the

engagement tool. The application of vacuum to the wafer is controlled between applied and released conditions to facilitate holding and release of the wafer.

### Wafer Input and Output Stations

Also mounted upon deck 23 are a wafer input station 43 and a wafer output station 44. Stations 43 and 44 inventory wafers being processed. Input station 43 holds an input wafer carrier 57 which contains a group of wafers which have been placed into the processing compartment for treatment. Output station 44 holds an output wafer carrier 58 which holds wafers which have been treated. Fig. 2 also shows a spray coating process station 40 and a thermal treatment station 46.

### Introduction to Process

The processing of wafers through processor 10 can be generally understood from Fig. 2 which will now be described. Wafers are fed to the system by opening processing compartment access door 24 and inserting input wafer cassette 57 loaded with wafers to be processed. The loading is typically done by manual insertion. As shown, the wafer cassette is oriented with the wafers in horizontal position. Wafers are individually removed from the input station wafer cassette 57 by the robotic wafer transfer mechanism 41. The wafers are transferred to the

1 spray coating station 40. In the spray coating station the wafers are  
2 spray coated according to the processes more fully explained below.

3 Wafer transfer 41 then removes the wafers from the spray coating  
4 station 40 and moves them to the thermal treatment station 46. In the  
5 thermal treatment station the wafers are most preferably heated to a  
6 desired heat treatment temperature and then cooled to a desired cold  
7 treatment temperature. In the preferred thermal treatment station 46,  
8 the heat treatment and cold treatment are carried out in distinct  
9 thermal treatment chambers. The wafer transfer mechanism 41 moves  
10 the individual wafers between the heating and cooling chambers within  
11 station 46.

12 After thermal treatment, the wafers are removed from thermal  
13 station 46 by wafer transfer 41. The spray coated and thermally  
14 treated wafers are then moved to the output wafer cassette 58. When  
15 the batch of wafers have been processed, the output cassette is removed  
16 via access door 24 and the processor 10 is ready to process another  
17 batch of wafers.

### 18 19 Spray Coating Station

20 Fig. 3 shows portions of the spray coating station 40 in greater  
21 detail. The spray coating station includes a processing head assembly  
22 49 which supports and rotates a wafer 50 being processed. The  
23 processing head is described in greater detail below, particularly in  
24 connection with Fig. 4. The processing head is constructed to mate

1 with a spray processing vessel bowl 51 to form a spray coating spray  
2 processing vessel 56. In the closed arrangement shown in Fig. 3, the  
3 processing head and processing bowl define a substantially enclosed  
4 processing chamber 63.

5 Processing head 49 is movable upwardly from the closed position  
6 shown in Fig. 3 to allow access through a processing bowl top opening  
7 59 through which wafer 50 and portions of the processing head are  
8 lowered. Processing head 49 is most preferably supported by a  
9 processing head shaft 80. Processing head shaft 80 is operated by a  
10 processing head operator 81 to both raise and lower the processing  
11 head. Processing head operator 81 is most preferably capable of both  
12 vertical motion and pivotal motion which causes shaft 80 to turn the  
13 processing head in a reciprocal manner between face-up and face-down  
14 positions. When the processing head is turned into a face-up position  
15 (not shown), the wafer 50 is positioned into the processing head with  
16 the wafer face-up. This is in comparison to the face-down position  
17 shown in Fig. 3. The back side of wafer 50 is adjacent to the  
18 processing head.

#### 19 20 **Spray Coating Station - Processing Vessel Bowl**

21 Fig. 3 shows that the preferred processing vessel bowl portion 51  
22 has a sidewall 52. Sidewall 52 is preferably cylindrical. As shown, the  
23 upper edge of the sidewall is provided with a top opening flange 54  
24 which surrounds and defines top opening 59. Flange 54 is provided

1 with a seal groove 55 which receives a suitable seal, such as an O-ring  
2 seal, therein for sealing between the processing head 49 and the  
3 processing vessel base or bowl 51.

4 Sidewall 52 is advantageously provided with a plurality of chamber  
5 cleaning nozzles 82 and 84. Nozzles 82 and 84 are preferably arranged  
6 in two levels, such as the upper level nozzles 82 and the lower level  
7 nozzles 84. The nozzles are positioned at suitable locations to allow  
8 solvent washing of the processing vessel interior surfaces. In the  
9 preferred construction there are two upper nozzles which are  
10 advantageously positioned at an angular spacing of 90°, at positions 0°  
11 and 90°. The two lower nozzles 84 are at 180° and 270° positions such  
12 that the nozzles are equiangularly spaced about the centerline. The  
13 position of nozzle 84 has been shifted in Fig. 3 for purposes of  
14 illustration. The chamber cleaning nozzles advantageously each have two  
15 nozzle openings to provide two jets which provide enhanced jet  
16 dispersion and greater spray washing effectiveness.

17 Fig. 3 also shows bowl 51 includes a frustoconical bottom bowl  
18 piece 53 which essentially defines the bottom wall of the processing  
19 vessel. The bottom wall also includes a drain having a drain fitting 60  
20 and drain opening 61. The bottom wall of the spray processing vessel  
21 also includes a spray assembly opening 62. Spray assembly opening 62  
22 receives portions of a spray assembly 70 therethrough. Spray assembly  
23 opening 62 is advantageously provided with a reinforcing boss 87 which  
24 defines the opening and is securely affixed to the bottom wall 53, such

1 as by welding. Spray assembly 70 produces a coating spray jet 69 of  
2 coating material and carrier gas which is directed onto the downwardly  
3 oriented face of wafer 50.

4 Fig. 3 also shows a processing bowl side compartment 78 which  
5 extends partially along one exterior side of the processing bowl 51.  
6 Side compartment 78 serves as a storage and nozzle cleaning  
7 compartment adjacent to the processing chamber 63. Compartment 78  
8 connects with processing chamber 63 via a storage compartment  
9 connection opening 88. A spray arm wash-down nozzle 79 is mounted  
10 near the top of the storage compartment. When a spraying operation  
11 or series of operations have been completed, the spray arm is pivoted  
12 into the storage compartment 78. The wash-down nozzle 79 is supplied  
13 with solvent to form a wash-down jet 109 which sprays solvent upon the  
14 spray-head 71 to, in particular, wash the coating spray nozzle 77. This  
15 prevents buildup of coating material at the nozzle 77 which may  
16 otherwise cause pluggage or adversely affect the coating application  
17 jet 69.

#### 18 19 **Spray Coating Station - Sprayer Assembly**

20 Fig. 3 shows the sprayer assembly in sectional view to indicate the  
21 preferred construction. Sprayer 70 includes a spray-head 71 which is  
22 movable within the processing chamber 63 to effect motion of coating  
23 spray nozzle 77. In the preferred construction shown, the spray swings  
24 about a pivot axis 105. This in combination with rotational movement

1 of the wafer 50 allows all areas of the downwardly facing surface of  
2 wafer 50 to be coated.

3 The elevational position of the spray head 71 is preferably  
4 adjustable. Fig. 3 shows spray-head 71 in the axially downward position.  
5 In this downward or removed position the spray-head is spaced relatively  
6 further from the wafer. A phantom line box illustrates spray-head 71  
7 in an alternative upward or close position when it has been moved  
8 upwardly into closer proximity to the wafer 50. The elevational or  
9 proximity position of the spray head relative to the surface being coated  
10 is adjustable within a range of differing proximity positions lying  
11 between a closest position and a remotest position. This allows the  
12 operator to optimize coating performance according to the requirements  
13 associated with a particular coating being used and other associated  
14 coating application parameters. As shown, the adjustment is  
15 accomplished using a manual adjustment mechanism which is described  
16 below.

17 Spray-head 71 is mounted upon a spray-head shaft 86. Spray-  
18 head shaft 86 forms part of a spray head actuator 85. Spray-head  
19 actuator 85 includes an outer support tube 90 which mounted upon the  
20 reinforcing boss 87, such as by threadably receiving the tube within the  
21 boss. A seal 89 is advantageously included near the upper end to seal  
22 between the boss and support tube. A pivot motor 91 is mounted  
23 upon the lower end of support tube 90, preferably using a motor  
24 mounting flange 107 which is connected to the support tube, such as



1 by welding. The pivot motor is fastened to flange 107 by fasteners  
2 (not shown).

3 Pivot motor 91 has an output shaft 92 which is connected by a  
4 coupling 93 to a pivot tube assembly 94. The pivot tube assembly also  
5 advantageously includes an angular position indicator arm 104 which is  
6 detected by a pivot position sensor 119 (Fig. 11) to indicate the pivot  
7 position for control of the pivot arm movement. Angular position  
8 indicator arm 104 is connected to a connection piece 103. Connection  
9 piece 103 is partially received in the upper end of the motor  
10 coupling 93. Connection piece 103 is preferably connected to the an  
11 outer pivot tube 95.

12 The pivot tube assembly includes outer pivot tube 95. Outer  
13 pivot tube 95 pivots within support tube 90. Outer pivot tube 95 is  
14 advantageously supported by bearings, such as the two bushing-type  
15 bearings 96. An annular spacer 97 extends between and spaces  
16 bushings 96. An outer seal 98 seals between pivot tube 95 and the  
17 inner diameter of support tube 90. An inner seal 99 seals between the  
18 spray-head support shaft 86 and the inner diameter of pivot tube 86.

19 Tubes 95 and shaft 86 pivot together in response to torque  
20 applied by the output shaft 92 of motor 91. The elevational position  
21 of shaft 86 is adjustable relative to outer pivot tube 95. Adjustment  
22 is accomplished by loosening a set screw 111 which is threadably  
23 received in a hole in outer pivot tube 95. Shaft 86 is then moved to  
24

1 the desired elevation or proximity position and secured by tightening set  
2 screw 111.

3 Pivot shaft 86 is made tubular to form a conduit passageway 112  
4 therethrough. The conduit passageway allows a coating conduit 113 and  
5 carrier gas conduit 114 to extend from the spray head nozzle block 120  
6 down passageway 112 for connection to related equipment described  
7 below. Conduits 113 and 114 extend through a lower conduit feed  
8 opening 115. The angular position of the spray assembly is detected  
9 by an angular position sensor 119 (Fig. 11) which optically or otherwise  
10 senses the position of arm 104.

11 Spray-head 71 includes a first spray arm part 101 which is  
12 secured to the upper end of pivot shaft 86. A second spray arm  
13 part 102 is connected to first part 101 to form a tubular arm which  
14 extends outward from shaft 86. Shaft 86 and spray arm 71 pivots  
15 about pivot axis 105.

16 Spray-head 71 also includes a nozzle assembly mounting head 118  
17 which is detachably connected to the distal end of second arm part 102  
18 using fasteners (not shown). The nozzle head 118 mounts a nozzle  
19 block assembly 120. Nozzle block 120 has a nozzle extension 121 which  
20 fits within a mounting aperture 122 formed in mounting head 118.  
21 Nozzle extension 121 contains the nozzle 77 through which coating and  
22 any carrier gas are emitted. Nozzle block 120 is provided with fittings  
23 123 and 124 which connect with the coating and carrier gas conduits  
24 113 and 114.

1        Nozzle block 120 is preferably a nozzle which provides good  
2 atomization of the coating liquid using a carrier gas. The preferred  
3 nozzle block has internal features which cause ultrasonic vibrations to  
4 be generated as the carrier gas passes through the nozzle block. The  
5 ultrasonic vibrations assist in providing good atomization of the coating  
6 with particle sizes in the range of 0.1-10 microns, more preferably on  
7 the order of approximately 1 micron in diameter. A suitable nozzle  
8 type is Sonicaire brand atomizing nozzle available from Ivek Corp. of  
9 North Springfield, Vermont.

10        Nozzle block 120 is preferably provided with nozzle block  
11 heaters 127 which are preferably electrical resistance heaters. The  
12 nozzle block heaters are preferably attached to both opposing sides of  
13 the nozzle block to heat the nozzle block and achieve an approximate  
14 desired temperature range. This serves in providing consistent viscosity  
15 control since the nozzle will be heated to an elevated temperature  
16 which stays approximately the same during operation. Suitable  
17 temperatures are in the approximate range of 20-150°C, more preferably  
18 30-100°C, even more preferably 40-80°C. Temperature can be controlled  
19 by varying the current passing through the nozzle block heaters.

20        Fig. 9 shows an alternative form of spray assembly according to  
21 the invention. In this view the spray arm head piece 118 has been  
22 substituted by an alternative three nozzle head piece 218. Head piece  
23 218 mounts three nozzle blocks similar to nozzle block 120. Each  
24 nozzle block has an emitting nozzle 77 and associated heaters. This

1 arrangement provides a more diffuse spray pattern. Otherwise the  
2 construction is similar with minor modifications associated with the  
3 increased number of nozzles.

#### 4 5 **Spray Coating Station - Sprayer Fluid Supply**

6 Fig. 10 shows a preferred system for supplying coating fluid and  
7 carrier gas to the nozzle block 120. Air, nitrogen or other suitable  
8 carrier gas is supplied from a facilities source via a cutoff valve 220.  
9 The gas then goes through a gas heater 221. A thermostatic control  
10 sensor 222 measures the temperature of the downstream gas passing  
11 through heater 221. Heater 221 is thus controlled to achieve a desired  
12 gas temperature. Alternatively sensor 222 can supply a signal to the  
13 central controller 300 (Fig. 11) and gas heater 221 can be used to  
14 controllably heat the carrier gas to a desired temperature. A pressure  
15 regulator 223 is downstream from heater 221 and is used to regulate  
16 the pressure of carrier gas being fed to nozzle block 120.

17 Fig. 10 also shows a coating fluid supply system. Coating is held  
18 in a coating reservoir 230. A control valve 231 can be included  
19 between the reservoir and pump 233. Pump 233 is preferably a  
20 precision controlled metering pump used with the preferred Sonicair  
21 brand nozzle described above and available from the same indicated  
22 source. The pump is controlled using a matching pump controller 235  
23 which controls the pump and its related electrical operating motor to  
24 provide the desired flow rate. Coating is supplied to the nozzle block

1 120 via coating conduit 113. Typical operating pressures are in the  
2 range of 5-100 pounds per square inch gauge pressure (psi), more  
3 preferably 10-30 psi.  
4

#### 5 Spray Coating Station - Processing Head

6 Fig. 4 shows The preferred construction for processing head 49.  
7 Head 49 is constructed similar to wafer processing head(s) shown and  
8 described in U.S. Patent No. 5,235,995, issued August 17, 1993 which  
9 is hereby incorporated by reference. Also pertinent are alternative  
10 processor head constructions shown and described in allowed U.S. Patent  
11 Application Serial No. 07/855,767 filed March 18, 1992, U.S. Patent No.  
12 \_\_\_\_\_, issued \_\_\_\_\_, which is hereby incorporated by  
13 reference. For purposes of convenience and facilitating the  
14 understanding of this invention without specific reference to such earlier  
15 patent, additional description is set out herein.

16 It should also be noted as a preliminary matter that the cutting  
17 plane used in Fig. 4 changes orientation at the centerline of the rotor  
18 to better illustrate additional features of the invention.

19 Processing head 49 includes a shroud 313 which forms a main  
20 structural part of the head and is connected shaft 80. Shaft 80 is  
21 mounted to shroud 313 using mounting rings 132 and fasteners (not  
22 shown). Shaft 80 is pivotable by a head operator 131 (see Fig. 2).  
23 Head operator 131 lifts shaft 80 and attached head 49 up and down.  
24

Operator 131 also pivots shaft 80. Pivoting shaft 80 causes the attached head 49 to flip between face-up and face-down positions.

Shroud 313 is generally disk-shaped. The outer edge of shroud 313 forms a rim 318. The face of shroud 313 has annular recesses 319 which receive portions of a wafer support piece 330 in proximity thereto. Wafer support piece 330 is mounted for rotation relative to shroud 313. Shroud 313 is also provided with a central opening through which portions of a motor support 358 are received.

Head 49 also has a housing 329 attached to shroud 313 in which the motor and other parts are enclosed. A top cap 360 is connected to the housing to further enclose the internal mechanical workings of head 49. The shroud, housing and cap are advantageously made of polyvinylidene fluoride or other suitable materials.

The processor head includes spacers or columns 326 which extend from lower motor mount 358 upwardly to support the upper mount 327. Spacers 326 have interior bores which receive fasteners (not shown) which extend through apertures formed through mount 327.

Processor head 49 also includes a wafer holder or support 330. Wafer support 330 is movably mounted to remaining parts of the head assembly to provide rotation or other appropriate relative motion between the wafer being processed and the spray assembly 71. The wafer support includes a disk-shaped wafer support plate 339 having an exposed downwardly directed front face and a upwardly directed back face removed from the wafer 50 being processed. The wafer support

1 plate 339 is advantageously constructed of polypropylene or other  
2 suitable material with an upturned flange 362 about the periphery  
3 thereof. Flange 362 can advantageously be provided with upwardly  
4 facing parallel extensions and associated grooves 363 to help restrict gas  
5 flow between flange 362 and shroud 319.

6 The wafer support 330 also includes a wafer support reinforcing  
7 wheel 390 which is secured within the wafer support piece 339 using  
8 a mounting ring 391. The reinforcing wheel 390 has a hub 392 to  
9 which is connected the output of motor 359. Such connection is  
10 described more fully below.

11 Wafer support 330 mounts a plurality of wafer support  
12 fingers 334, such as the four shown, or more. The wafer support  
13 fingers 334 have distal ends 337 which are formed to provide gripping  
14 notches 338 in which the peripheral edge of wafer 50 is held. The  
15 distal ends of support fingers 334 are spatially contracted toward one  
16 another to hold wafer 50, or expanded outwardly to release the wafer.

17 Fig. 4 shows that wafer support fingers 334 are flexibly mounted  
18 by finger bushings 335 to allow deflection thereof and the relative  
19 expansion and contraction needed for controlled gripping and release of  
20 wafer 50. Finger bushings 335 are preferably integrally formed with  
21 fingers 334. The finger bushings have an enlarged diameter exposed  
22 surface flange 321 which faces downwardly toward wafer 50. The finger  
23 bushings are held in position by a retaining ring 322 mounted to engage  
24 the back or upper surface of wafer support plate 339. The exposed,

1 lower face also in part defines an annular web or diaphragm 323 which  
2 provides the flexibility needed to allow fingers 334 to pivotally deflect  
3 between expanded and contracted positions. The finger bushings 335  
4 are made of a flexible material, such as TEFLON or other material  
5 suitable for service in the chemical environment which exists within  
6 processing chamber 63.

7 The wafer support fingers 334 also have upper or proximate  
8 ends 341 which are provided with connection receptacles 325. The  
9 connection receptacles receive end pieces 342 therein to form a  
10 mechanical coupling. End pieces 342 are displaced laterally by finger  
11 connection rods 344 to tilt the end pieces and attached wafer support  
12 fingers. The tilting action causes the relative expansion and contraction  
13 of the distal ends of the support fingers in the triad arrangement.

14 Actuation of the support fingers is advantageously accomplished  
15 using finger actuators 343. The finger actuators 343 each include a  
16 connecting rod 344 which is pivotally connected at a first or outer end  
17 to an end piece 342. The inner or second ends of connecting rods 344  
18 are pivotally connected to a remote end of a positioning link 345. The  
19 opposite or mounted ends of positioning links 345 are pivotally  
20 connected to the wafer support plate 339 using positioning link  
21 brackets 347. The positioning links 345 are oriented at oblique angles  
22 extending inwardly from the pivotal connections with the brackets 347  
23 toward the remote ends and the pivotal connections with connecting  
24 rods 344. The positioning links 345 can be provided with biasing



1 | springs 387 which urge links 345 upwardly and the associated wafer  
2 | fingers 334 into contracted positions tending to grip the wafer.

3 |       The wafer support fingers are moved into expanded positions to  
4 | release the wafer by displacing the pivotal joints between connecting  
5 | rods 344 and positioning links 345 downwardly and inwardly. This  
6 | causes the connecting rods to move inwardly in a radial direction to  
7 | displace the proximate ends of the wafer fingers inwardly and the  
8 | opposite distal ends outwardly to release the wafer. The connecting  
9 | rods are displaced downwardly and inwardly by an annular contact  
10 | ring 351. Contact ring 351 is operated by a pair of small pneumatic  
11 | pistons 349. Pistons 349 are slidable within cylindrical piston  
12 | cylinders 350 formed in motor support 358. Pressurized fluid is  
13 | supplied to the upper sides of pistons 349 to force them downwardly  
14 | and cause contact between annular contact ring 351 and connecting  
15 | rods 344.

16 |       The wafer support piece 339 is also advantageously provided with  
17 | a set of four standoffs 382 which serve to support wafer 50 during  
18 | loading of the processing head. Wafer 50 is loaded with the head in  
19 | a face-up position with the distal end of the standoffs available to be  
20 | contacted by the backside of wafer 50.

21 |       The wafer support drive assembly includes a motor 359 which is  
22 | mounted upon motor support 358. Motor 359 is preferably a brushless  
23 | DC motor. Motor 359 has a hollow motor shaft 353 supported by a  
24 | set of ball bearings 355. The hollow motor shaft 353 receives a

1 detachable shaft 354 therethrough. Detachable shaft 354 is threadably  
2 connected to a shaft head 383. Shaft head 383 includes an enlarged  
3 flange 356. The shaft head is connected to the motor shaft to rotate  
4 therewith using a pin (not shown) or other suitable means. The  
5 flanged head is received within a shaft head receptacle 368 formed in  
6 the back surface of hub 392. Spaced, axially oriented, anti-rotation  
7 pins 357 are engaged between the lower face of the flanged shaft  
8 head 356 and corresponding holes formed in receptacle 368. A snap-  
9 ring retainer 369 holds the flanged head 356 axially within  
10 receptacle 368.

11 The angular positions of fingers 334 about the rotating assembly  
12 rotational axis X-X are preferably controlled to assume desired positions  
13 when the rotatable wafer support 330 stops. This indexing of the  
14 stationary positions of fingers 334 is needed when the processing head  
15 is opened to provide proper engagement of the wafer by the robotic  
16 transfer unit engagement head.

17 A preferred indexing means 250 used to position the wafer  
18 support, motor and other rotatable parts forming the rotating assembly  
19 of the processing head drive. Rotor positioning or indexing  
20 mechanism 250 includes a multi-sided cammed rotor plate 259 mounted  
21 to rotate with motor shaft 353 using coupling 271. The cam plate 259  
22 has a plurality of sides equal in number to the number of fingers 334.  
23 Each side of rotor plate 259 has a curved edge configuration. The  
24 curved configurations of each of the three side segments are sloped

relative to a circle defined by axis X-X. The curves slope from high points at the adjoining ends of the side segments toward central low points. The central low points serve as a detent when engaged by an edge engagement roller (not shown) which is controllably forced inward. When motor 359 is inoperative and the motor shaft is freely rotatable, the inward force of the roller causes rotor plate 259 to pivot to bring the rotating assembly into an angular position which centers the roller within a low point of the cammed rotor plate.

A motion monitoring assembly is also advantageously provided within processing head 49 for measuring the speed and direction of rotation of the wafer plate 330 about the rotational axis X-X. The motion monitoring assembly includes a rotor indicating element, such as rotor indicator disk 254. Indicator disk 254 is provided with a series of peripheral notches which intermittently pass and interrupt one or more optical beams and associated sensors (not shown).

#### **Wafer Thermal Treatment Station**

Figs. 6-8 show a preferred form of thermal treatment station 46. Thermal treatment station 46 includes three bays or receiving chambers 221-3. Receiving bays 221-3 are designed to each receive a single wafer which has been coated in the spray coating station 40. The top and bottom receiving bays 221-2 are associated with thermal treatment units in the form of wafer heaters 225. The middle receiving bay 223 is provided with a thermal treatment unit in the form of a

1 wafer cooler. The wafer heaters and cooler are constructed similarly.  
2 The preferred construction of both will now be described with specific  
3 reference to a wafer heater 225. The difference between the heaters  
4 and cooler will be noted in the description.

5 Fig. 8 shows a preferred wafer heater 225. A wafer 50 is  
6 positioned upon the upper surface of a platen 226. Platen 226 is  
7 preferably constructed with features that improve heat transfer between  
8 wafer 50 and the platen. More Specifically, the upper or contact  
9 surface 227 of the platen is formed to fit against the back surface of  
10 wafer 50. As shown, wafer 50 and the contact surface 227 have flat  
11 complementary contacting surfaces. The platen is preferably made from  
12 a metal of good thermal conductivity, such as aluminum. The contact  
13 surface of the platen is also preferably provided with a network or  
14 array of vacuum aperture grooves 228. As shown, vacuum apertures  
15 228 are constructed as three concentric grooves which are controllably  
16 connected to a vacuum supply and supplied with vacuum pressure when  
17 the wafer is to be held in position upon platen 226. The vacuum  
18 pressure applied over the back side of wafer 50 pulls the wafer into  
19 better contact with the platen thus improving heat transfer. Vacuum  
20 is supplied to grooves 228 via vacuum conduits (not shown) formed in  
21 the platen.

22 The wafer heater is also preferably provided with a thermal  
23 source element 230 which is mounted to contact the back surface of  
24 platen 226. In the wafer heater 225 the thermal source element 230

1 is a serpentine electrical resistance heater. In the wafer cooler used  
2 for bay 223, the thermal source element is an array of cooling passages  
3 (not shown) through which are circulated a cooling fluid. Alternatively,  
4 a thermoelectric cooler or other suitable cooling apparatus formed in  
5 the shape of a relatively thin layer.

6 Thermal treatment unit 225 also has an insulatory back piece 231  
7 which extends over the back of the platen and interposed heater or  
8 cooler 230. Insulation piece 231 is preferably formed of a suitable  
9 ceramic material having relatively good thermal insulating properties.  
10 A variety of suitable materials are available.

11 The platen 226, thermal source element 230, and insulating  
12 piece 231 are backed with a support plate 232. A fastener 234 is  
13 advantageously used to assembly these pieces. Fastener 234 is provided  
14 with male threads along its length and is received within mounting  
15 apertures formed in all four of the pieces. The mounting aperture in  
16 platen 226 is threaded. A spacer 235 is positioned adjacent the back  
17 support plate 232 and serves to space between plate 235 and a radiant  
18 shield plate 236 which reduces radiant heat transfer. The lower end  
19 of fastener 234 is received in a she-bolt 237 having internal female  
20 threads. The lower end of she-bolt 237 is fastened to the unit frame  
21 piece 238 using fastener 239. Thermal unit 235 preferably uses four  
22 assembly mountings as just described.  
23  
24

1 Thermal treatment unit 225 also has a lifting mechanism 240 for  
2 lifting wafer 50 from the surface of the platen. Lifting mechanism 240  
3 includes a lifting actuator. The lifting actuator preferably includes a  
4 stepper motor 241 which has an output shaft which mounts a circular  
5 or other suitable cam 242. Cam 242 is eccentric upon the output shaft  
6 to controllably raise and lower a cam follower 271. Cam follower 271  
7 is advantageously a rotatable bearing with associated outer race which  
8 contacts cam 271. Cam follower 271 is connected to an actuator  
9 plate 243 which moves up and down with controlled angular movement  
10 of the motor 241. Three lifting rod assemblies 245 are held in the  
11 platen assembly in a tripod arrangement. The lifting rod assemblies are  
12 contacted by the actuator plate and are moved upwardly and  
13 downwardly in response to operation of actuator 241.

14 Lifting rod assemblies 245 include a contact rod 246. Contact rod  
15 246 is provided with an enlarged head 247 which is mounted for linear  
16 travel in a lifting rod receiving pocket 248. The contact rod also  
17 connects with a connector 249 which is slidably received through  
18 apertures formed through the back piece 232 and heat shield 236. A  
19 lift biasing spring 252 is compressed between the underside of shield  
20 236 and a connector contact head 251. Spring 252 biases the contact  
21 rod upwardly to lift wafer 50. Actuator 240 overpowers the biasing  
22 springs to retract the contact rods downwardly. The rods can be fully  
23 or partially retracted to achieve contact or a desired proximity of the  
24 wafer to the platen 227.

## Control System

Fig. 11 shows a schematic presentation of the preferred control system. In such there is a central controller 300 which is connected to various control system components which are either activated or provide sensory input information. Many alternative control system configurations are possible. As shown, the wafer transfer 41, touch screen display 31, disk drive 32, stop switch 33, keyboard port 34, spray arm motor 91, pump controller 235, thermal treatment station operator 221, processing head 49, head operator 131, thermal treatment station lift 240, and spray pivot sensor 119 are shown connected to the central controller.

## Methods and Operation

The invention further includes novel methods for processing microelectronic or semiconductor articles to provide a coating thereon. The preferred methods are directed to processing methods which can provide a coating which conforms to surface irregularities which are necessarily a part of chemically etched or otherwise irregularly formed surface topologies.

In one form of the invention, the novel methods preferably include loading one or more wafers or other semiconductor articles into a processing enclosure. This is advantageously accomplished by opening the access door 24 and loading an input wafer cassette 57 into the input station position 43. The methods further advantageously include

1 closing the access door and thereby substantially enclosing the processing  
2 compartment 15.

3 The preferred methods also advantageously can include transferring  
4 a wafer from the input station. This transferring is accomplished by  
5 inserting a wafer engagement tool, such as tool 67, into juxtaposition  
6 with wafer 50 and applying a vacuum force to effect holding of the  
7 wafer upon the engagement tool. The transferring also preferably  
8 includes moving the wafer from the input station by moving the wafer  
9 transfer apparatus 41.

10 The novel methods also preferably include positioning a wafer or  
11 other article within a spray processing vessel. This is done in the  
12 processing system 10 by loading the semiconductor article being coated  
13 into the spray coating station 40 and closing the processing vessel parts.  
14 Loading is preferably effected by lifting or raising the processing head  
15 49. Loading further advantageously includes pivoting the wafer holding  
16 processing head into a face-up position to receive the wafer thereon.  
17 Loading also can include expanding the wafer engagement fingers into  
18 open positions to receive the wafer 50 therebetween, and then closing  
19 the fingers into engaging positions which hold the wafer. The loading  
20 phase further preferably includes pivoting processing head 49 into a  
21 face-down position adjacent to the processing vessel bowl 51. The  
22 processing vessel is then effectively closed by lowering or otherwise  
23 bringing the processing head into complementary relationship with the  
24 vessel bowl. Assembling the processing head and bowl together in



1 conjoined relationship produces a substantially enclosed processing  
2 chamber 63 in which the wafer is coated.

3 In preferred forms of the invention the novel methods further may  
4 include rotating or otherwise moving the wafer. This is accomplished  
5 in processor 10 by rotating the processing head motor and attached  
6 wafer support piece 136. The rotating step is preferably accomplished  
7 at rotational speeds in the range of 1-1000 revolutions per minute, more  
8 preferably 10-300 revolutions per minute, even more preferably 50-200  
9 revolutions per minute.

10 The methods further include spraying the wafer or other  
11 semiconductor or microelectronic article which has been positioned within  
12 the processing vessel. Spraying is accomplished while moving the spray  
13 head assembly 71. The moving of the spray head causes the nozzle or  
14 nozzles 77 to move relative to the article being coated. The spray  
15 head assembly is preferably pivoted to cause the relative movement  
16 between the nozzle 77 and the wafer surface. The rotational speed and  
17 relative movement of the nozzles are coordinated to achieve a uniform  
18 conformal layer of coating material.

19 In preferred methods according to this invention, the spray arm  
20 is advantageously started in a radial position outboard of the piece  
21 being coated. The spray can be started from the nozzle in an  
22 outboard position to reduce or eliminate any transitory startup effects  
23 before the coating spray contacts the wafer surface. Thereafter the  
24 spray arm is pivoted so that nozzle or nozzles 77 are swept to or

1 through the rotational axis of the wafer. This movement of the spray  
2 nozzles is coordinated so that the coating application rate density is  
3 uniform over the area being coated. In the preferred methods the  
4 radial velocity of the nozzles relative to the wafer rotational centerline  
5 is increased as the nozzle position moves toward the center of rotation.  
6 Conversely, as the nozzle moves outwardly during any return spraying  
7 process, the radial velocity decreases. The nozzle path velocity is  
8 ideally a function which is inversely proportional to the radial position  
9 of the nozzle relative to the rotational centerline of the wafer. Even  
10 more preferably, the nozzle path velocity is a function which is inversely  
11 proportional to the square of the radial position of the nozzle.

12 The coordinated application step also considers the application rate  
13 which is precisely controlled to effect metering of the spray coating  
14 liquid. This metering is performed in system 10 by the coordinated  
15 operation of spray pump 233, pump controller 235, and associated  
16 carrier gas flow rate. In the coating of semiconductor wafers, liquid  
17 coating pump rates in the approximate range of 1-1000 microliters per  
18 second are potentially useful, more preferably 5-300 microliters per  
19 second, even more preferably 10-100 microliters per second. The  
20 coating flow rate to the nozzles is most preferably kept at a constant  
21 or nearly constant rate during the spraying operation. This has been  
22 found advantageous in providing stable operation.

23 The methods according to this invention also preferably use carrier  
24 gas flows which provide significant coating particle velocities. Increased

1 coating particle velocities aid in impacting the particles against the  
2 surface of the wafer or other article being coated to provide better  
3 conformal coating application.

4 It may be preferable in some coating applications to utilize carrier  
5 gases which participate in or are specifically inert to the chemistry  
6 involved. For example, in the application of polyimide coatings it has  
7 been found desirable to utilize nitrogen instead of air. The processing  
8 chamber is preferably purged with nitrogen and the carrier gas used is  
9 also nitrogen. This reduces chemical effects upon the polyimide which  
10 are associated with moisture which is present in air supplies even when  
11 treated to reduce or remove moisture. In other situations the carrier  
12 gases used may enhance or retard coating setup rates and may be  
13 desirable with the particular coating being applied.

14 In some forms of the invention, novel methods include heating the  
15 carrier gas which is used in the spraying. This heating is effected in  
16 the preferred embodiment using heater 221. The spraying also  
17 preferably includes regulating the carrier gas pressure. Pressures in the  
18 range of approximately 0-25 pounds per square inch gauge are believed  
19 appropriate, more preferably carrier gas pressures are regulated to be  
20 in the approximate range of 5-15 pounds per square inch gauge. The  
21 volume of carrier gas can vary from none to relatively high flow rates  
22 depending upon the coating being applied. The figures given above are  
23 for nozzles having an approximate orifice diameter in the range 1/8-1/16  
24 inch.

1 The spraying also preferably includes generating a sonic vibratory  
2 resonance within the spray block to cause atomizing to be performed  
3 to achieve the approximate coating particle sizes indicated above. The  
4 generating of vibratory resonance is preferably effected by passing the  
5 carrier gas through a suitable nozzle structure, such as the ultrasonic  
6 nozzle explained above.

7 Spraying according to the novel methods of this invention also  
8 advantageously includes controlling the viscosity of the coating liquid  
9 being applied. This controlling is advantageously effected by heating the  
10 coating to achieve greater stability with regard to viscosity fluctuations.  
11 The heating is best done by heating the nozzle block 120 using the  
12 heaters 127. The controlled heating of the carrier gas is also a  
13 relevant parameter in achieving control of the coating viscosity.

14 The preferred methods may also advantageously include providing  
15 a purge of gas along the back side of wafer 50. This purging of the  
16 atmosphere along the wafer back side helps to prevent coating overspray  
17 from settling and adhering to the back side of the wafer. Such a  
18 purging function is accomplished with a gas purge port (not shown)  
19 which supplies purge gas to the back side of support piece 339 and an  
20 aperture which is formed through support piece 339 at a desired  
21 location.

22 The methods of this invention further include removing or  
23 unloading the coated wafer or other semiconductor article from the  
24 processing chamber. This is advantageously accomplished by opening the

1 processing vessel. Opening the processing vessel includes lifting or  
2 otherwise removing the processing head 49 from the processing bowl 51.  
3 It further preferably includes pivoting the processing head to turn the  
4 wafer into a coated-side-up or face-up position.

5 Unloading also preferably includes engaging the wafer with the  
6 wafer engagement tool in the same or very similar manner described  
7 above with regard to transferring the wafer from the input station.

8 The coated wafer is then preferably transferred to a thermal  
9 treatment station, such as thermal treatment station 46. This is done  
10 using the wafer transfer 41. The process of transferring the wafer also  
11 includes loading or installing the wafer into a thermal treatment  
12 receiver, such as either of the heating treatment chambers 221 or 222.  
13 During loading of the thermal treatment chambers, the wafer contact  
14 members 246 are extended. Thus the extending step should be  
15 performed before installing the wafer into the thermal treatment  
16 chamber. The wafer transfer functions by gently lowering the wafer  
17 onto the contact members. Thereafter the engagement tool functions  
18 by retracting from the thermal treatment chamber. The thermal  
19 treatment unit then functions by lowering the lifting mechanism 240.  
20 The lowering or moving into proximity can result in a desired proximity  
21 spacing, such as 0.5-1 millimeter. In other coating applications it may  
22 be preferred to perform the positioning by contacting the wafer against  
23 the platen 226 by fully retracting the contact members 246. The wafer  
24

is then subjected to vacuum by applying vacuum pressures via channels 228 which causes a forcing of the wafer against the platen.

The methods further preferably include transferring heat relative to the wafer. In the most preferred methods the heat transferring includes both heating and cooling. The heating step is preferably accomplished first. The heating is effected by activating the heater 225 to heat the platen and allow heat to flow from the platen to the wafer. The heating is preferably performed for sufficient time to render the coating mechanically stable upon the surface of the wafer. The time needed to accomplish this will vary depending on the coating and wafer being coated. In many situations, the heat treatment time will be in the range of 1-10 minutes, more preferably 1-3 minutes. Thereafter the vacuum pressure is reduced thereby releasing the force applied by the vacuum. The wafer is then readied for removal by lifting or otherwise extending the wafer using the wafer lifting mechanism.

After the heating step, the wafer is then most preferably transferred from a heating chamber 221 or 222, to the cooling chamber 223. The loading process is the same or similar to that described above in connection with the heating chamber. The cooling treatment process is also very similar to that described above for the heating process. The cooling treatment in general requires about one-half the time required for the heat treatment curing of the coating. Thus the need for only one cooling unit for two heating units.

After the coated wafer has been coated, and then heated, cooled or both, it is again transferred by wafer transfer 41. The wafer transfer moves the wafer to the output station 44. At the output station, the wafer transfer performs by inserting the wafer into the output station carrier 58 in an available space therein. When all wafers of a batch have been completed, the output wafers are removed by opening the access door and manually removing the carrier.

In compliance with the statute, the invention has been described in language more or less specific as to structural and methodical features. It is to be understood, however, that the invention is not limited to the specific features shown and described, since the means herein disclosed comprise preferred forms of putting the invention into effect. The invention is, therefore, claimed in any of its forms or modifications within the proper scope of the appended claims appropriately interpreted in accordance with the doctrine of equivalents.

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2	<b>System Generally</b> . . . . .	7	<b>Spray Coating Station - Processing Vessel</b>
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4	control side or section 12 . . . . .	7	top opening flange 54 . . . . .
	wafer processing side or section 13 . . . . .	7	seal groove 55 . . . . .
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23	spray processing vessel 56 . . . . .	12	first spray arm part 101 . . . . .
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	processing head shaft 80 . . . . .	12	nozzle extension 121 . . . . .
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